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A Simulator-Based Analysis of Engineering Treatments for Right-Hook Bicycle Crashes at Signalized Intersections

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- A Simulator-Based Analysis of Engineering Treatments for Right-Hook Bicycle Crashes at
- Signalized Intersections
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- *Keywords:* Bicycle safety; Driver behavior; Driving simulator; Intersection design; Engineering
- treatment; Right-hook crash
-

ABSTRACT

 A right-hook crash is a crash between a right-turning motor vehicle and an adjacent through- moving bicycle. At signalized intersections, these crashes can occur during any portion of the green interval when conflicting bicycles and vehicles are moving concurrently. The objective of this research was to evaluate the effectiveness of four types of engineering countermeasures – regulatory signage, intersection pavement marking, smaller curb radius, and protected intersection design – at modifying driver behaviors that are known contributing factors in these crashes. This research focused on right-hook crashes that occur during the latter stage of the circular green indication at signalized intersections with a shared right-turn and through lane. Changes in driver performance in response to treatments were measured in a high-fidelity driving simulator. Twenty-eight participants each completed 22 right-turn maneuvers. A partially counterbalanced experimental design exposed drivers to critical scenarios, which had been determined in a previous experiment. For each turn, driver performance measures, including visual attention, crash avoidance, and potential crash severity, were collected. A total of 75 incidents (47 near-collisions and 28 collisions) were observed during the 616 right turns. All treatments had some positive effect on measured driver performance with respect to the right- turn vehicle conflicts. Further work is required to map the magnitude of these changes in driver performance to crash-based outcomes.

1. Introduction

 Cycling is viewed as an integral component of the multimodal transportation system in the long-range plans of many cities in the United States. As cities have invested in nonmotorized transportation infrastructure to realize this goal, bicycling has become a meaningful alternative mode of transportation for commuting to activities such as school, work, shopping, and recreation (Pucher et al., 1999, 2006, 2011). However, even with these investments, safety remains an important issue. In 2011 alone, there were 677 bicyclist fatalities and 48,000 bicyclist injuries in the United States (NHTSA, 2013). One of the more prevalent bicycle-motor vehicle crash types at intersections is the *right-hook crash*, a collision that occurs between a right-turning vehicle and an adjacent through-moving cyclist. Between 2007 and 2011, right-hook crashes represented over 500 of reported crashes involving cyclists and 59% of all bicycle-motor vehicle crashes at signalized intersections in Oregon (Hurwitz et al., 2015). Many more crashes or near misses are not reported. Therefore, this type of crash is a safety concern for bicyclists. There are some published insights into the causal factors behind these crashes. The Institute of Transportation Engineers (ITE) reported that in nearly 70% of bicyclist-motor vehicle collisions at intersections, the motorist reported that "they did not see the bicyclist before the collision" (ITE, 2004). In an earlier phase of this research, Hurwitz et al. (2015) reported that failures in the situational awareness of the driver significantly contributed to the occurrence of right-hook crashes. Specifically, the driver failed to look for the bicyclist, looked but did not see the bicyclist, or looked and saw the bicyclist but failed to predict their behavior accurately. Treatments that improve conspicuity of the bicyclist within the intersection may help to reduce

the frequency of right-hook crashes.

 The objective of this research was to determine the effectiveness of four types of engineering countermeasures (regulatory signage, intersection pavement marking, smaller curb radius, and protected intersection design) at modifying driver behaviors (driver visual attention, crash avoidance, and potential crash severity) that are known to contribute to right-hook crashes. Participants completed a series of right-turn maneuvers in a high-fidelity, motion-based driving simulator. A partially counterbalanced experimental design exposed drivers to critical scenarios. For each turn, driver performance measures were collected and analyzed to determine the effects of treatments on the occurrence of right-turn vehicle conflicts.

 We previously identified the highest situational risk factors for drivers and cyclists, including the most common intersection geometries for right-hook crashes occurring in the state of Oregon (Hurwitz et al., 2015). In this paper, we analyzed driving simulator experiments under these critical conditions. We evaluated driver behaviors in collisions that occur during the latter green phase at signalized intersections with a bicycle lane and a shared right-turn and through lane. The term "latter green phase" refers to the second portion of the green signal phase, after the initial vehicle queue has cleared and the green signal indication is still displayed.

2. Literature review

 There are many different types of engineering treatments related to bicycle safety, but very few have been identified or evaluated specifically for the right-hook crash scenario. This section reviews the known effects of pavement marking, signage, and geometric design features as they relate to bicycle-motor vehicle crashes.

2.1. Signage

 The only right-hook crash signage approved by the U.S. *Manual on Uniform Traffic Control Devices* (MUTCD) is the R4-4 "Begin Right Turn Lane, Yield to Bikes" sign, which is meant to inform roadway users of the merging maneuver at signalized intersections with an exclusive right-turn lane and a bike lane (FHWA, 2009). The Oregon Department of Transportation (ODOT, 2013) suggests an additional option, the ODOT OR10-15b "Turning Vehicles Yield to Bikes" sign, applicable to the mitigation of right-hook crashes occurring at signalized intersections with a shared right-turn and through lane.

 Right-hook crash signage is often used in conjunction with another right-hook crash treatment, such as colored pavement markings. The National Association of City Transportation Officials (NACTO) *Urban Bikeway Design Guide* states that "A 'Yield to Bikes' sign should be used at intersections or driveway crossings (with colored pavement marking) to reinforce that bicyclists have the right-of-way at colored bike lane areas". This guide provides three alternative designs that are variations of existing MUTCD-approved signage (NACTO, 2011a). The City of Portland, OR (1999) found that the additional "Yield to Bikes" sign was a critical aspect of the effectiveness of blue pavement marking (intended to help roadway users identify the potential conflict area), as "substantially more motorists who noticed the sign correctly identified the meaning of the blue area". The authors suggested that the supplementary sign is even more important than the blue pavement markings, due to its clarification of the regulatory message and the prioritized right-of-way. In another study by Brady et al. (2011), however, the signage did not appear to alleviate driver confusion over the appropriate yielding behavior. The researchers reported a reduction in driver yielding after installation of a similar sign. They concluded that driver confusion would likely occur over whether to cross the green-colored bicycle lane or to cross after the colored section.

2.2. Pavement markings

 Laboratories (ASL) eye-tracking system (Caird et al., 2008). Although results for two of the four treatments were not presented, the authors showed that a blue skipped pavement marking treatment resulted in a higher yielding rate (90%) than a sharrow symbol treatment (77%).

2.3. Geometric design

 Effects of geometric elements on right-hook bicycle crashes are not well documented. Reduction of the curb radius is a key element that has the potential to improve bicyclist safety at intersections by slowing down turning vehicles. This reduced velocity lessens the severity of collisions if they do occur and provides more time for the motorist or bicyclist to perform an avoidance maneuver. Multiple guidance sources recommend the use of smaller corner radii to improve pedestrian safety in a similar manner, but do not provide bicycle-specific curb radius design guidance (*ODOT, 2011; NACTO, 2013).*

 Another, relatively novel, geometric design treatment for bicycle safety is the "protected" or Dutch-style intersection. Protected intersections incorporate a specific combination of geometric design and traffic engineering features to increase bicyclist safety and visibility. Literature regarding this design treatment largely comes from Europe, where these intersections are more common. For example, Goeverden and Godefrooij summarized before-and-after case studies of bicycle-related infrastructure interventions in the Netherlands. The common theme of these case studies was the redesign of intersections with respect to geometric design elements that are similar to those of protected intersections. Although these changes led to significant improvements in the perceived safety of the facilities, this effect "was not fully reflected by the observed decrease in accidents and casualties". However, because the Dutch bicycle infrastructure is already fairly well integrated into the Dutch transportation system, other

 countries may see "different (probably larger) impacts" (Goeverden and Godefrooij, 2011). At present, there is little U.S. guidance for protected intersections, although this situation is likely to change. The *Separated Bike Lane Planning & Design Guide*, recently released by the Massachusetts Department of Transportation (MassDOT, 2015), prominently features and describes protected intersections and associated best practices.

3. Methodology

 To address the gaps in knowledge identified in the literature review and to mitigate the causal factors for right-hook crashes that were identified in a previous experiment (Hurwitz et al., 2015), we designed a second experiment to test various design treatments and controls in a simulated driving environment under specific environmental conditions. We examined and analyzed motorist behavior, including the right-turning motorists' visual attention, crash avoidance behavior, and potential crash severity, in response to four different categories of possible right-hook crash treatments.

3.1. Driving simulator

 The Oregon State University (OSU) Driving Simulator is a high-fidelity, motion-based simulator consisting of a full 2009 Ford Fusion cab mounted above an electric pitch motion 165 system. This system is capable of rotating $\pm 4^{\circ}$ and allows for the commensurate representation of acceleration or deceleration*.* Three projectors display a front view of 180°. A fourth projector displays a rear image for the driver's center mirror. Two side mirrors of the vehicle cab have embedded LCD displays. Simulator software records performance measures (e.g., velocity, position, and acceleration) at a sampling rate of 60 Hz. The virtual environment is created by

- using typical simulator software packages (Internet Scene Assembler and SimCreator) and
- design software (AutoCAD Civil 3D and Blender). Figure 1 shows views of the simulated
- environment from outside (a) and inside (b) of the vehicle.
-

 Fig. 1 Views from (a) outside and (b) inside the OSU Driving Simulator. (c) Researcher wearing the eye-tracking device.

3.2. Eye tracker

 Eye movement consists of fixations and saccades. Fixations occur when the gaze is directed towards a particular location and remains still for some period of time (Green, 2007; Fisher et al., 2011)*.* Saccades occur when the eye moves from one point to another. The Mobile Eye-XG eye-tracker system (Fig. 1c) was used to collect information about the visual fixations and glance patterns of participants at a sampling rate of 30 Hz with an accuracy of 0.5°–1.0°. The participant's gaze was calculated from the correlation between the position of the pupil and the reflection of three infrared lights on the eyeball. The system recorded a fixation when the participant's eye paused in a certain position for more than 100 ms. For this research, only fixations were analyzed.

188 *3.3. Treatment options*

189 Four independent treatment variables were selected: signage, pavement marking, curb 190 radius, and protected intersection design. Each independent variable was either dichotomous or 191 categorical in nature and had two, three, or five levels (Table 1).

192

193 **Table 1**

194 Experimental Factors and Levels.

Protected intersection with islands and green pavement markings

3.4. Research hypotheses

 The visual attention of motorists was measured by eye-movement fixation data, collected with a head-mounted mobile eye-tracker. The potential influence of experimental treatments on right-turning motorists' eye movement formed the basis of the research questions regarding the visual attention of motorists. The first research hypothesis was established to guide the assessment of visual attention for each individual treatment:

- *H0*: The engineering treatment has no effect on the right-turning motorist's mean total fixation duration on areas of interest (AOIs) in the driving environment.
- Motorist performance was assessed with the global performance measure of crash avoidance during right-turning maneuvers in the latter portion of the green indication and in the presence of bicyclists at a signalized intersection. The consideration of crash avoidance behavior for intersection approaches with different treatments helped to determine the relative impact of the alternative treatments. The second research hypothesis was established to guide the assessment of crash avoidance behavior for each individual treatment: *H0*: The engineering treatment has no effect on the right-turning motorists' time-to-
- collision (TTC) values at the time of near-collisions or collisions.
- Potential crash severity of incidents was measured by vehicle velocities, which were collected by the driving simulator. Higher velocities at the time of the traffic conflict were

considered to be more severe, as injuries to the cyclist generally increase with higher velocities.

By considering vehicle velocities for intersection approaches with different treatments, we were

able to determine the relative impact of alternative treatments. The third hypothesis was

established to guide the assessment of crash severity for each individual treatment:

 H0: The engineering treatment has no effect on the right-turning motorist's velocity at the time of near-collision or collision.

3.5. Experimental design

 Environmental loading factors were selected by considering our previous findings regarding the causal factors of right-hook crashes at this type of signalized intersection configuration (2015). According to our results, the combined presence of oncoming turning vehicles and a bicyclist approaching from behind at a high speed (16 mph) was the worst-case casual scenario for right-hook crashes. In each of the experimental right-turn scenarios, the participant would experience the following environmental loading characteristics: 228 1. The signal would change to green before the driver approached the intersection, 229 creating a "latter green phase"; 2. An oncoming vehicle would turn left as the participant approached the intersection, and two more vehicles would be waiting in the oncoming lane with their turn signals illuminated; 3. Within fairly close proximity to the intersection, a bicyclist would appear in the

driver's blind zone on the roadway, specifically located in the bicycle lane; and

- 4. The bicyclist would travel at a constant speed of 16 mph through the intersection,
- subsequently forcing the driver to yield the right of way, increase their speed to pass in front of the cyclist, or collide with the cyclist.

The cross-section of the roadway included two 12-ft. traffic lanes, with 6-ft. bicycle lanes

in each direction. Intersection approaches included a single shared right-turn and through lane

and a single receiving lane. Intersection approaches had posted speed limits of 35 mph. Fig. **1**

shows an example of an intersection approach in the simulated environment as it was presented

to the participant.

Fig. 1. Screen capture of an intersection approach in simulated environment.

 To measure the influences of the treatment alternatives, participants were exposed to various treatment configurations. The experiment was a factorial design with 24 scenarios presented across six grids. Signage (two levels), pavement marking (five levels), and curb radius treatments (two levels) were fully counterbalanced against one another, resulting in 20 scenarios. Due to the design characteristics of this treatment, protected intersection treatment was only

 counterbalanced against signage treatment, resulting in four scenarios. Due to a coding error, two of the 24 scenarios were duplicated and the protected intersection treatment was not counterbalanced with the signage treatment. Therefore, the experiment included 22 unique scenarios across all treatments. This duplication was taken into consideration during the analysis of the resulting data.

 Fig. **2** shows an example of the grid layout of four right-turning scenarios. The orange arrow "path" indicates the sequence of intersections that participants were asked to drive through. An automated voice command instructed participants to "Turn right at the next intersection". To control for practice or carryover effects, the order of the intersection grids was counterbalanced. In this randomized partial counterbalancing procedure, six different grid sequences were chosen and randomly presented to participants.

Fig. 2. Example of grid layout with four right-turning (RT) scenarios. Grid 5 Path: Start-Right-

Right-Right-Thru-Right-Right-Right-Finish.

3.6. Participant demographics

treatment intersections were lost across seven participants. As each treatment was only presented

290 once to each participant, the remaining participants' data were still considered useable (a total of

291 596 right-turn maneuvers).

292

- 293 Table **2** summarizes the AOIs that were considered in the analysis of visual attention. Fig. **3**
- 294 presents an annotated illustration of the AOIs. Although drivers were free to turn their heads, and
- 295 although the simulator included rear-vision projection, true blind-spot checks were not possible.

296 However, no subject in the simulator turned their head while making a turn.

297

298 **Table 2**

299 Summary of AOIs.

- Average total fixation duration (ATFD) was calculated for each AOI and each treatment
- variable. ATFD provided a quantitative measure of how the motorist's visual attention was

306 distributed across targets (Fisher et al., 2011). Table 3 presents the ATFD values for all AOIs,

307 aggregated by treatment level.

308

309 **Table 3**

Treatment Type Level Bicyclist Bicyclist Side Mirror Rear Mirror Bicyclist $\frac{\text{Side}}{\text{Area}}$ Mirror Mirror Rear Turning Signal Pavement Marking Prot. Int. Island Signage Signage S0 0.63 0.50 0.35 0.48 0.63 2.16 0.98 1.21 0.62 S1 0.57 0.42 0.42 0.48 0.56 1.85 0.94 1.18 1.07 Pavement Marking PM0 0.64 0.48 0.31 0.55 0.58 2.01 1.15 1.07 PM1 0.75 0.42 0.31 0.41 0.68 2.23 0.93 1.31 PM2 0.62 0.42 0.35 0.51 0.50 1.93 0.94 1.10 PM3 0.60 0.40 0.44 0.46 0.68 1.92 0.72 1.34 PM4 0.45 0.53 0.39 0.47 0.58 1.92 1.01 1.17 Curb Radius C0 0.58 0.46 0.41 0.52 0.62 1.93 0.90 1.15 1.29 C1 0.63 0.45 0.35 0.44 0.56 2.10 0.99 1.24 1.25 Protected Frotected
Intersection PI1 PI0 (T1) 0.62 0.43 0.28 0.62 0.71 1.97 1.24 PI0 (T11) 0.50 0.40 0.51 0.45 0.46 1.56 0.55 1.9 PI1 0.49 0.69 0.59 0.62 0.69 2.44 1.06 1.62 PI2 0.57 0.57 0.36 0.71 0.34 2.01 1.01 1.07 PI2 0.50 0.40 0.51 0.45 0.46 1.56 0.55 1.07

310 Summary of ATFD Values for All AOIs.

311

 Fixation data were statistically analyzed by a two-sample Welch's t-test for all AOIs by comparing ATFDs for the level-zero condition and each non-zero level condition. ANOVA was used to identify significant differences between ATFDs for the zero-level and non-zero levels. Results of these statistical analyses are presented in Table 4. ATFD distributions for the AOIs were strongly skewed to the right. Data were log-transformed, and zero values (i.e., data for participants who did not look at the AOI) were removed from the analysis. Thus, the statistical tests represent the subgroup of drivers who looked at the particular AOIs. 319

320 **Table 4**

Treatment Type	Level	Bicyclist Side Mirror	Bicyclist Rear Mirror	Bicyclist	Side Mirror	Rear Mirror	Turning Vehicle	Signal	Pavement Marking	Prot. Int. Island	Signage
Signage	S ₁	0.46	0.07	0.31	0.88	0.66	$0.001*$	0.53	0.42	0.13	N/A
Payement Marking	PM1	0.37	0.96	0.89	0.07	0.28	0.57	$0.01*$	N/A	N/A	0.49
	PM ₂	0.85	0.79	0.53	0.44	0.63	0.79	0.15	N/A	N/A	0.54
	PM ₃	0.43	0.56	0.23	0.28	0.09	0.47	$0.001*$ N/A		N/A	0.50
	PM4	$0.03*$	0.30	0.35	0.33	0.64	0.75	0.21	N/A	N/A	0.94
Curb Radii C1		0.31	0.57	0.45	$0.04*$	0.93	0.21	0.38	0.50	N/A	0.76
Protected Intersection PI2	PI1	0.68	0.15	$0.02*$	0.96	0.82	0.56	0.65	N/A	N/A	N/A
		0.48	0.67	0.38	0.19	0.27	0.17	0.13	N/A	N/A	0.19

321 Summary of Statistical Analyses of ATFD Values.

322 * Statistically significant differences ($p \le 0.05$).

323

332

333 **Table 5**

334 Summary of Motorist Fixations on Bicyclist.

336 *4.1.1. Discussion*

 For the crash potential metric, signage treatment had the greatest effect on behavior. Fig. 5. shows the ATFDs with 95% confidence intervals on the 11 AOIs for the signage treatment levels (S0, no signage present and S1, signage present). A generally positive pattern of change was observed between ATFDs for the two levels of signage treatment. ATFDs for the Side Mirror and Bicyclist in Side Mirror AOIs increased with S1 treatment. Drivers spent 9–10% more time scanning for the bicyclist in the side mirror with the S1 treatment than they did with the S0 treatment.

346

 This result indicates that the S1 treatment may positively influence driver behavior. The message of the sign may alert the driver that they should be actively looking for a bicyclist while approaching the intersection. This may also be enhanced by the trend of the driver's visual path towards the right side of the road when the S1 treatment is present. The driver is already looking in that direction, and it may feel natural to continue moving the visual scanning path to the right, towards the passenger side mirror. This possibility would also explain the 14% reduction in ATFD for the Rear Mirror AOI with the presence of additional signage (0.30 vs. 0.35 s). The only statistically significant difference in ATFDs occurred for the Turning Vehicle AOI (two-tailed p-value = 0.001 for S0 vs. S1). Motorists spent less time fixating on oncoming turning vehicles with the S1 treatment than they did with the S0 treatment (1.85 vs. 2.16 s). This

 change could influence the ATFDs for bicyclist-related AOIs, in that a greater portion of their visual attention could have been allocated to the ATFDs for those bicyclist-related AOIs. However, all of the bicyclist-related AOIs either decreased or remained the same. ANOVA revealed that fixations on the oncoming turning vehicles had statistically significant differences 361 in ATFDs ($p = 0.001$). No other statistically significant differences were found.

4.2. Crash avoidance

 We evaluated treatments with respect to crash avoidance by analyzing simulator output data collected while participants drove through 22 right-turning intersections. The primary objective of this experiment was to determine how well motorists were able to detect the potential hazard (i.e., bicyclist in the adjacent bicycle lane) and avoid a crash with the bicyclist while performing the right-turn maneuver. Crash avoidance was measured by considering motorists who could not avoid a near-collision or collision with the through-moving adjacent bicyclist lane. The bicyclist approaching the intersection from behind the motorist was entirely within the motorist's blind spot. The participant could avoid collision by detecting the bicyclist in the rear or side mirror. The three-dimensional display in the driving simulator did not show vehicles immediately to the right of the motorist, and participants had a larger blind spot than in a real driving environment (Gugerty, 1997). Placement of the bicyclist in the experimental coding was such that the motorist would likely hit the bicyclist approaching from the vehicle's blind spot unless the bicyclist was detected in the mirrors (i.e., a worst-case loading situation). Motorist crash-avoidance behavior was observed during every right-turn maneuver. Motorists driving in the simulated environment were observed continuously from the simulator's operator station and by the participant's head-mounted mobile eye-tracker. Eye-tracker video

 records were analyzed, and the crashes and near-collisions were noted. Recorded crash data were validated by checking the locations of the subject vehicle and bicycle centroids, recorded as dynamic variable data in the driving simulator. We assessed crash avoidance behavior using descriptive statistics and statistical analysis, similarly to the prior driver measures.

 During the 616 right turns, 75 incidents (47 near-collisions and 28 collisions) were made across 21 treatments by 20 participants. Thirteen participants (65%) crashed more than once. Crash factors comprised both environmental and motorist factors; however, only environmental factors were assessed for this study. TTC was calculated for right-turn maneuvers that resulted in incidents. Traffic conflicts between a right-turning motorist and a through-moving bicyclist were defined as instances when a collision would be imminent if the trajectories remained unchanged. TTC was calculated when the centroid of the turning vehicle crossed the bicycle's path. Because the bicycles were coded to have constant speed, this measure of the TTC value was fixed (i.e., there was no dynamic nature of the TTC value as neither actor could adjust the collision course). Because TTC was calculated from the vehicle centroid, our results are not necessarily comparable to other experiments with more careful calculation of TTC values from vehicle edge to vehicle edge. Results showed that 57% of traffic conflicts had TTCs equal to or less than 1.5 s (Fig. 6).

Fig. 6. TTC frequency and cumulative frequency distributions for all incidents.

 The risk of collision (ROC) score was determined by classifying TTCs of 0.0–0.9 s as "high risk" and TTCs of 1.0–1.5 s as "moderate risk". According to the TTC threshold values 403 and ROC scores, only 26 of the 75 incidents had high-risk ($n = 8$) or moderate-risk ($n = 18$) TTC values (Brown, 1994; Gettman et al., 2008; Sayed et al., 1999).

 The dataset was split by the four independent treatment variables, to isolate their individual impact. Frequency and cumulative frequency distributions were plotted for the various treatment levels. Cumulative frequency represents the percentage of incidents with TTCs below 0.9 or 1.5 s (as specified) among the total number of incidents at a specific treatment level. All treatments had incidents with TTC values greater than 1.5 s; however, for brevity, not all results are shown here. As an example, Fig. 7 shows frequency and cumulative frequency distributions for the curb radius treatment levels (C0, 30-ft. curb radius and C1, 10-ft. curb radius). A Chi-square test was performed for treatments to test for any statistically significant differences between ROC scores of the various treatment levels. Because the ROC scores were

directly calculated from the TTC values, this statistical analysis reflects the significance of

415 differences in the TTC value bins within the frequency and cumulative frequency distributions.

417

420

421 **Table 6**

422 Summary of Statistical Analysis for ROC Scores of Near-collisions and Collisions.

424 *4.2.1. Discussion*

425 For the crash avoidance metric, protected intersection designs had the greatest effect on 426 behavior but showed an inconsistent pattern of change. Protected intersection treatment levels 427 were unique because the treatment was not fully counterbalanced with the other treatments. PI0 428 (T1) and PI0 (T11) corresponded to base intersection treatments with 30-ft. curb radius and no 429 pavement marking, without (T1) or with signage (T11). PI1 and PI2 were protected intersection 430 treatments with islands and 30-ft. curb radius, either with no signage and no pavement marking 431 (PI1) or with signage and green pavement marking (PI2). Figure 8 demonstrates the frequency 432 and cumulative frequency distributions for protected intersection treatment levels.

434 **Fig. 4.** TTC frequency and cumulative frequency distributions by protected intersection

435 treatment level.

```
437 Cumulative frequencies of high-risk TTC values (\leq 0.9 \text{ s}) were lower with PI1 vs. PI0
438 (T1) (31% vs. 50%) and with PI2 vs. PI0 (T11) (45% vs. 60%), but cumulative frequencies of 
439 moderate- and high-risk TTC values (\leq 1.5 \text{ s}) were higher with PI1 vs. PI0 (T1) (55% vs. 50%)
```
 and PI2 vs. PI0 (T11) (73% vs. 60%). Chi-square test results revealed no statistically significant differences at the 95% confidence level (Table 6). Overall, the impact of the protected intersection treatment on crash avoidance behavior was inconsistent. However, the reduction in high-risk TTC values could indicate that the physical separation of the barrier island at the corner of the protected intersection creates more space/time between the driver and bicyclist.

4.3. Potential crash severity

 Treatments were evaluated with respect to potential crash severity to determine the effects of selected engineering treatments on the velocity of motorists when a near-collision or collision occurs with the bicyclist during the right-turn maneuver. Bicyclists traveled at the same velocity (16 mph) throughout the experiment, but the vehicle velocities varied across participants and treatments. For this potential crash severity analysis, the only velocities considered were those of vehicles at the time of moderate- or high-risk traffic conflicts (determined by the TTC values). Higher velocities at the time of the traffic conflict were considered to be more severe. Figure 5 displays a boxplot and scatterplot distribution of the vehicles velocities across all of the moderate- and high-risk incidents. As can be seen in the figure, there is a single outlier in this data (with a velocity equal to 5.03 mph). This outlier was removed for calculation of the mean and range values of the vehicle velocities, which are summarized in Table 7. The mean velocity for these "moderate risk" and "high risk" incidents was 12.70 mph and the range of the vehicle velocities was 8.57 mph.

461 **Figure 5** Boxplot and scatterplot of vehicle velocities for all moderate- & high-risk incidents

 A two-sample Welch's t-test and the ANOVA analysis were performed to compare the zero-level with non-zero treatment levels. Table 7 displays mean velocities of the moderate- and high-risk incidents for the treatment levels and the resulting p-values. The PI0 (T1) treatment had only one moderate- to high-risk incident; thus, statistical tests could not be performed. No statistically significant differences were found at the 95% confidence level. 468

469 **Table 7**

470 Summary of Statistical Analysis for Vehicle Velocities of Near-collisions and Collisions.

4.3.1. Discussion

 For the crash potential metric, curb radius treatments had the most effect on behavior. This treatment is particularly important for the potential crash severity measurement, as a smaller curb radius generally requires a slower turning velocity. Fig. **6** displays a boxplot and scatterplot distribution of the vehicle velocities across all moderate- and high-risk incidents for the curb radius treatment levels (C0, 30-ft. curb radius and C1, 10-ft. curb radius). The single outlier in 478 the C0 data (velocity $= 5.03$ mph) was removed for the calculation of the mean and range values of the vehicle velocities for this treatment level.

 The C1 radius treatment led to a 4% smaller mean vehicle velocity (12.33 mph) and a 54% smaller range of vehicle velocities (10.76–14.47 mph; difference: 3.71 mph) than the C0 radius treatment (mean: 12.90 mph; range: 8.88 – 16.98 mph; range difference: 8.10 mph). This reduction in vehicle velocities, while anticipated due to the fundamental concepts of geometric design, is a clear safety benefit. Lowering the speeds of turning vehicles by any amount will reduce the severity of a potential collision. P-values for the ANOVA analysis and Welch's t-test 490 were both 0.63. Thus, there were no statistically significant differences between C0 and C1, as measured by vehicle velocities at the time of the incident, at the 95% confidence level.

5. Conclusions

5.1. Overall findings from this study

 This research evaluated the effects of design treatments (supplemental signage, intersection pavement marking, curb radius, and protected intersection design) on motorist behavior using three different motorist performance measures: visual attention of motorists, their crash avoidance behavior, and the potential severity of the near-collision or crash, as measured by the motor vehicle speed. All performance measures were assessed during right-turn maneuvers that occurred during the latter portion of the green phase at signalized intersections with a shared right-turn and through lane, under the highest driver-loading scenario identified in our prior experiment. Most of the differences were not statistically significant; however, the lack of a statistically significant effect for a particular treatment does not necessarily mean that the treatment will not have an effect on safety. Our interpretations of the data and recommendations, with respect to the four treatment types, follow.

5.1.1. Signage treatments

 Findings of this experiment indicated that the level-one signage treatment, the ODOT OR10-15b "Turning Vehicles Yield to Bicycles" symbol sign (Table 1), is an effective method of positively influencing driver behavior with respect to visual attention. We found a generally positive pattern of change in visual attention with the addition of the sign. Participants increased the amount of time spent scanning the side mirror for the bicyclist by 9% and the side mirror when in close proximity to the intersection (i.e. when the bicyclist is visible within the side mirror) by 10% compared to the level-zero signage treatment.

5.1.2. Pavement marking treatments

 We found mixed results with respect to the influence of pavement markings on changes in driver behavior. The presence of through intersection markings improved measured driver performance in the visual search and crash avoidance spectrums. Although all tested designs had some positive effects, our evidence suggested that either the single or double dotted white bike line with bicycle stencil pavement marking (level-one or level-two treatment) should be considered. The addition of green markings, commonly associated with bicycles, did not change the driver's visual attention as much as the simpler, white dotted line markings.

5.1.3. Curb radius treatments

 The smaller curb radius treatment (10-ft. radius, level-one treatment in Table 1) appears to be an effective method of positively influencing driver behavior, with respect to crash avoidance and potential crash severity. We found a generally positive pattern of change in potential crash severity with the addition of the smaller curb radius, with a 4% decrease in mean vehicle velocity during moderate- to high-risk incidents compared to the larger curb radius. With the level-one curb radius treatment, the range of vehicle velocities was 54% less than the range with the level-zero treatment. This finding of lower speeds is consistent with the formulaic relationship between the design speed and the minimum radius of curvature, found in "A Policy on Geometric Design of Highways and Streets" of the American Academy of State Highway and Transportation Officials (AASHTO, 2011).

5.1.4. Protected intersection treatments

 Protected intersection treatments included no protected intersection (level zero), protected intersections with islands (level one), and protected intersections with islands and green pavement markings (level two) (Table 1). Level-one protected intersection treatment appears to be an effective method of positively influencing driver behavior with respect to potential crash severity. We did not find a consistent pattern of change in crash avoidance with the addition of the protected intersection with islands. Level-one treatment led to a 19% lower cumulative 544 frequency of high-risk TTC values $(\leq 0.9 \text{ s})$ and 5% higher cumulative frequency of moderate-545 and high-risk TTC values $(\leq 1.5 \text{ s})$ than the level-zero protected intersection treatment.

 We did not find the level-two protected intersection treatment to be a consistently effective method of positively influencing driver behavior. We did not observe a consistent pattern of change in crash avoidance with the addition of the protected intersection with islands and green pavement markings. This treatment resulted in a 15% lower cumulative frequency of high-risk TTC values and 13% higher cumulative frequency of moderate- and high-risk TTC values than the level-zero protected intersection treatment. Frequencies of moderate- and high- risk TTCs with the level-two treatment were significantly lower than with the level-one protected intersection treatment (5 vs. 19 and 3 vs. 15, respectively).

5.2. Recommendations

 Every treatment had some positive measurable effect on driver performance. The presence of signage improved driver performance across the visual attention spectrum. The sign attracted the driver's attention and resulted in more frequent searching for bicyclists. Given its relatively low cost, the "Turning Vehicles Yield to Bicycles" sign should be installed where feasible. To maximize the effect, the sign should be installed in a location most visible to drivers and in advance of the turning-merge conflict area. Use of a smaller curb radius produced decreases in the vehicle turning speed and the number of high-risk conflicts. The reduction in vehicle turning speed was expected but is a clear measured benefit for safety. Pavement markings, particularly the simplest dotted markings, also improved most driver behaviors. We did not observe sufficiently significant changes to recommend the use of additional green markings; however, our results are not conclusive and we do not intend that our recommendation be construed to suggest that the green markings not be installed.

 Protected intersections with an island and/or green pavement marking would require further design work. The consideration of many issues (e.g., constructability issues, truck turning/mountable curbs, reflective markings on curbs for visibility at night, and accommodation of pedestrians) was outside the scope of this study. Nonetheless, the protected intersection designs did show some improvements in driver performance with respect to the potential crash severity as measured by vehicle speeds in near and actual collisions. This finding correlates with the curb radius treatment. The protected intersection design differs from other treatments in that it moves the conflict point between the car and bicycle forward in the intersection. Finally,

 unlike the other treatments, the protected intersection was a novel design that was not familiar to any driver.

5.3. Limitations and future work

 This research provides valuable insights on the causal factors of right-hook crashes during the latter portion of the green phase at signalized intersections. Although various driver performance metrics can be measured robustly, it is not yet clear how to map the magnitudes of differences to expected crash outcomes. One fundamental limitation of the within-subject design is fatigue effects, which can cause the participant's performance to decline over time during the experiment. Participants might get tired or bored as the experiment progresses. Furthermore, repeated right-turning maneuvers pose the threat of inducing simulator sickness more frequently than through movements in simulated driving. To reduce the risks of fatigue effect and simulator sickness, the experiment could be conducted in two trials on two different days.

 Another limitation associated with this study is related to the statistical power of the analyses. According to post-hoc power calculations, limited statistical power was observed which could be due to the limited number of observations.

 Oregon driving code and practices involve striping bicycle lanes all the way to the intersection, which differ from practices in other states. Drivers living in Oregon will likely understand these designs, which might differ for drivers elsewhere. The experiment could be conducted in other states to see whether these and other behavioral differences exist. Finally, this experiment measured the performance of individual treatments, either alone or in combination with other treatments. No analysis was performed to identify the optimal combination.

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